

Simulating thermodynamics ensembles

what you simulate is what you would measure

Marcus Elstner and Tomáš Kubař

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Intro

- system of classical particles interacting with potential V
 - **deterministic system**
- given **initial conditions** (\vec{r}_0 and \vec{v}_0),
trajectory of the system ($\vec{r}(t)$ and $\vec{v}(t)$)
is determined for all of the future $t \rightarrow \infty$
- for some systems – **analytic** solution
e.g. harmonic oscillator:

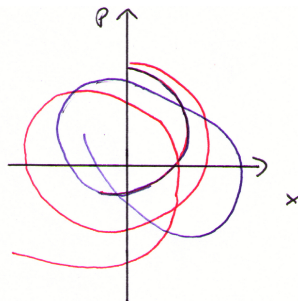
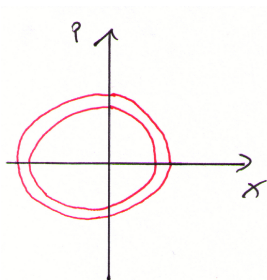
$$x(t) = x_0 \cdot \cos[\omega t] \qquad v(t) = -v_0 \cdot \sin[\omega t]$$

Intro

- for a complex system – trajectory is obtained **numerically**
- so-called **chaotic** systems – strictly deterministic, too
- chaos – two trajectories close in phase space initially will depart exponentially from each other (solution of the eqns of motion is **unstable**)

Intro

stable and unstable solutions of eqns of motion



Intro

stochastic process – when we do not have sufficient information about all of the degrees of freedom of the system

then, we have to describe the systems with **statistical mechanics**

what we need – techniques to control basic simulation parameters
– temperature, possibly pressure etc.

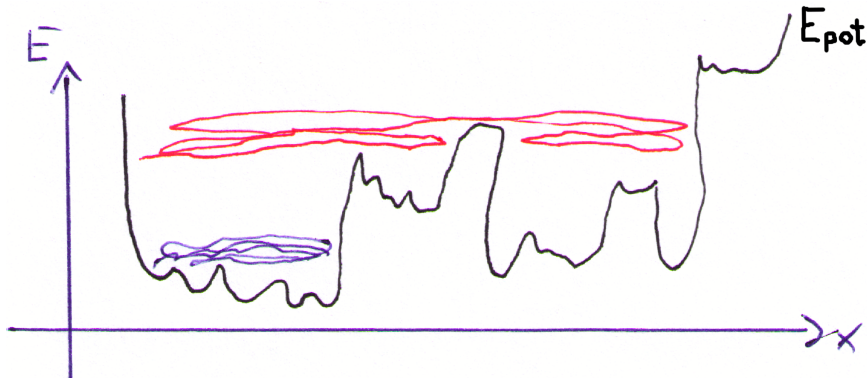
T – determines if a region of phase space shall be reached in MD
phase space – different sampling at high and at low temperatures
– different ensembles will be generated

particularly important – to find a way to model the system,
so that we obtain correct phase space density at a given T

Intro

high E – multiple different regions of the phase space are reached

low E – restricted available region of phase space



difference $E - E_{\text{pot}}$ corresponds to E_{kin} and temperature

Isolated system

- exchanges with surroundings neither energy (heat / work)
nor matter (particles)
- total energy of system: $E = E_{\text{kin}} + E_{\text{pot}} = \text{const}$
- individually, E_{kin} and E_{pot} fluctuate in the course of time
as they are being transformed into each other
- is what we get when using the Verlet method for a molecule
- trajectory in the **microcanonical ensemble**

Isolated system

kinetic theory of gases \rightarrow relation of E_{kin} and temperature:

$$\langle E_{\text{kin}} \rangle = \frac{3}{2} NkT$$

$$\text{where } \langle E_{\text{kin}} \rangle = \frac{1}{2} \sum_i m_i \langle v_i^2 \rangle$$

$$\text{so } T = \frac{\sum_i m_i \langle v_i^2 \rangle}{3Nk}$$

'local' / 'instantaneous' temperature

$$T = \frac{\sum_i m_i v_i^2}{3Nk}$$

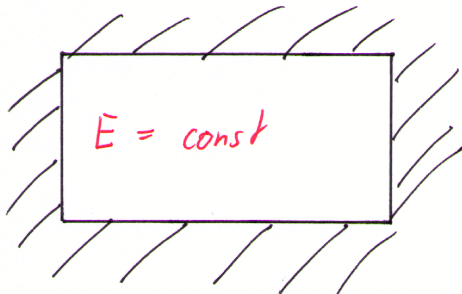
- fluctuates in time
- may differ between different parts of system

Isolated and closed system

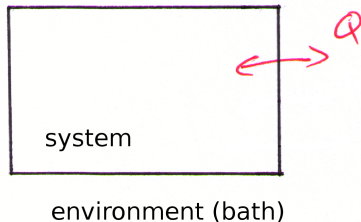
experimental setup (a test tube with a sample)

- usually in **thermodynamic equilibrium** with the surroundings
- temperature (and optionally pressure) equal as that of surr.

isolated system



closed system



Closed system

- thermal contact of system with surroundings
- exchange of energy in the form of heat
 - until the temperature of surroundings is reached
- strictly speaking: T only defined with such thermal contact
(\rightarrow N/A in case of isolated system)
- MD simulation of such a system will provide
a trajectory in the **canonical ensemble**

Canonical ensemble

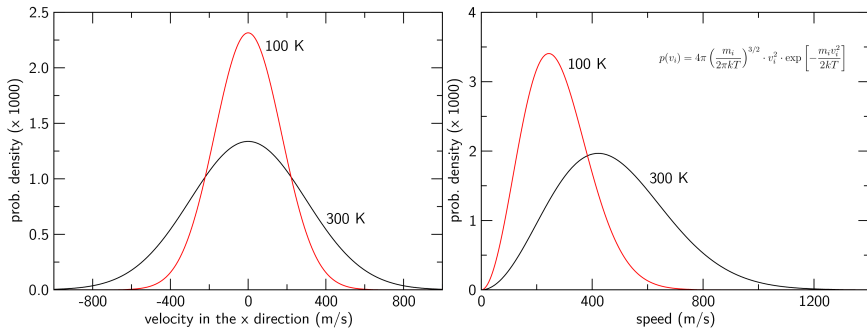
velocity / speed of atoms – Maxwell–Boltzmann distribution

$$p(v_{x,i}) = \sqrt{\frac{m_i}{2\pi kT}} \cdot \exp\left[-\frac{m_i v_{x,i}^2}{2kT}\right]$$

$$p(v_i) = 4\pi \left(\frac{m_i}{2\pi kT}\right)^{3/2} \cdot v_i^2 \cdot \exp\left[-\frac{m_i v_i^2}{2kT}\right]$$

Canonical ensemble

velocity / speed of atoms – Maxwell–Boltzmann distribution



(for N_2 as IG)

Equipartition theorem

(Gleichverteilungssatz) (DoF = degree of freedom)

Every DoF contains the same average amount of kinetic energy of

$$\left\langle \frac{1}{2} m_i v_{x,i}^2 \right\rangle = \frac{1}{2} kT$$

Each atom i has 3 DoF x_i , y_i and z_i (and $v_i^2 = v_{x,i}^2 + v_{y,i}^2 + v_{z,i}^2$) \rightarrow

$$\langle E_{\text{kin}} \rangle = \left\langle \sum_i \frac{1}{2} m_i v_i^2 \right\rangle = \left\langle \sum_i \frac{1}{2} m_i v_{x,i}^2 + \frac{1}{2} m_i v_{y,i}^2 + \frac{1}{2} m_i v_{z,i}^2 \right\rangle = \frac{3}{2} NkT$$

Such a distribution of velocity and kinetic energy is a property of systems in contact with heat bath (not of isolated system)

Attention if constraints are being applied:

- reduced number of DoF $3N - N_c$ here and in all what follows!

Equipartition theorem

Virial theorem:

$$\left\langle \sum_k q_k \frac{\partial H}{\partial q_k} \right\rangle = \left\langle \sum_k p_k \frac{\partial H}{\partial p_k} \right\rangle = \left\langle \sum_k p_k \frac{dq_k}{dt} \right\rangle = - \left\langle \sum_k q_k \frac{dp_k}{dt} \right\rangle$$

(DoFs: generalized coordinates q_k , generalized momenta p_k)

Generalized equipartition theorem – extension of virial theorem:

$$\begin{aligned} \left\langle p_k \frac{\partial H}{\partial p_k} \right\rangle &= kT \rightarrow \left\langle \frac{1}{m} p_k^2 \right\rangle = \frac{1}{2} kT \\ \left\langle q_k \frac{\partial H}{\partial q_k} \right\rangle &= kT \rightarrow \langle q_k \cdot F_k \rangle = -kT \\ &\rightarrow \langle \vec{r}_i \cdot \vec{F}_i \rangle = -3kT \end{aligned}$$

How can we **control** the temperature in simulation?

Naïve thermostat – scaling of velocities

in a Verlet MD simulation – ‘instantaneous temperature’ T deviates from the target T_{ref} (of bath = the surroundings)

$$T(t) = \frac{2}{3} \frac{E_{\text{kin}}(t)}{Nk} \neq T_{\text{ref}}$$

$T(t)$ – another designation for E_{kin} determined by velocities

a simple idea – **scale** the velocities by a certain factor λ :

$$\begin{aligned} T_{\text{ref}} &= \frac{1}{\frac{3}{2}Nk} \cdot \frac{1}{2} \sum_i m_i (\lambda \cdot v_i)^2 = \\ &= \lambda^2 \cdot \frac{1}{\frac{3}{2}Nk} \cdot \frac{1}{2} \sum_i m_i v_i^2 = \lambda^2 \cdot T \end{aligned}$$

scaling of all velocities by $\lambda = \sqrt{T_{\text{ref}}/T} \rightarrow T_{\text{ref}}$ reached exactly

Naïve thermostat – scaling of velocities

- very crude way of controlling the temperature
- rescaling of velocities affects the ‘natural’ way of evolution of the system
- velocities – not sure if the distribution is correct (M–B)
- importantly, system does not sample any canonical ensemble
 - phase space density is not that of a canonical ensemble
 - very important because everything is calculated as averages:

$$\langle A \rangle = \frac{1}{Z} \int \rho \cdot A \, d\vec{r} d\vec{p}$$

- possibly: wrong sampling \rightarrow wrong averages

Naïve thermostat – scaling of velocities

How to avoid the drastic changes to the dynamics?

adjust velocities more smoothly, in the direction of T_{ref} ,
resigning on T_{ref} to be recovered in every step immediately

Berendsen thermostat

- system coupled to infinite bath with temperature T_{ref}
- temperature changes between two time steps according to

$$\frac{dT}{dt} = \frac{1}{\tau} (T_{\text{ref}} - T)$$

- exponential decay of temperature towards T_{ref} :
- rate of change of T (due to the change of velocities)
is proportional to the deviation of actual T from T_{ref} ;
constant of proportionality – relaxation time τ
- change of temperature due to thermostat, during 1 time step:

$$\Delta T = \frac{\Delta t}{\tau} (T_{\text{ref}} - T)$$

Berendsen thermostat

$$\Delta T = \frac{\Delta t}{\tau} (T_{\text{ref}} - T)$$

- to achieve ΔT , velocities are scaled by λ as above:

$$\begin{aligned} T_{\text{new}} &= T + \Delta T = T + \frac{\Delta t}{\tau} (T_{\text{ref}} - T) \\ \lambda &= \sqrt{\frac{T_{\text{new}}}{T}} = \sqrt{1 + \frac{\Delta t}{\tau} \left(\frac{T_{\text{ref}}}{T} - 1 \right)} \end{aligned}$$

- usually: $\tau = 0.1 - 10$ ps
- T is still fluctuating – however around the desired value T_{ref}

Berendsen thermostat

fluctuation of temperature – desired property
for canonical ensemble – **variance** of ‘inst. temperature’ T :

$$\sigma_T^2 = \left\langle (T - \langle T \rangle)^2 \right\rangle = \langle T^2 \rangle - \langle T \rangle^2$$

and relative variance

$$\frac{\sigma_T^2}{\langle T \rangle^2} = \frac{2}{3N}$$

large number of atoms N : fluctuations $\rightarrow 0$
finite-sized systems: visible fluctuation of temperature

- feature of the canonical ensemble
- we would not obtain this with the simple velocity scaling

Berendsen thermostat

drawbacks:

- correct canonical ensemble is still not generated!
- various parts of the system (different individual molecules, or solute \times solvent) may exhibit different temperatures, while the temperature of the entire system is 'correct'
 - may remain like that for extended periods of time
- gradually moves the energy from the fastest modes of motion to the slowest/weakest ones, **violating the equipartition**
 - the fastest – bond stretching and angle bending
 - loss of energy \rightarrow 'freezing' of the molecules
 - the slowest – 3 transl'ns (+ 3 rot'ns) of the entire system
 - energy gain \rightarrow 'flying (+ spinning) ice cube'

Nosé–Hoover thermostat

- conceptionally and mathematically > difficult to understand
- heat bath is treated not as an external element
rather as an integral part of the system
- the **bath** – an additional DoF **s** with fictitious mass **Q**
may be understood as time-scaling parameter:

$$dt' = s \cdot dt$$

- eqns of motion will be propagated for this **extended** system,
for which an energy-like quantity will be conserved
- generates canonical NVT ensemble of the molecular system!

Nosé–Hoover thermostat

expression for the energy of the system involves the bath:

$$E_{\text{pot}} = U(r) + g \cdot kT_{\text{ref}} \cdot \log s$$

- g – number of DoF of the system = $3N + 1$
- T_{ref} – reference temperature

$$E_{\text{kin}} = \sum_i \frac{1}{2} m_i s^2 \dot{r}_i'^2 + \frac{1}{2} Q s'^2$$

- attention needed – derivatives w.r.t. the modified time:

$$dt' \neq dt \rightarrow \dot{r}_i' \neq \dot{r}_i$$

Nosé–Hoover thermostat

- eqns of motion for the extended system ($3N + 1$ DoF)
derived with the **Hamiltonian formalism**:

$$H(r', \dot{r}', s, \dot{s}') = E_{\text{pot}} + E_{\text{kin}}$$

- eqns for the molecular DoF:

$$\frac{dr_i}{dt'} = \frac{1}{m_i} \cdot \frac{\partial H}{\partial \dot{r}'_i} \qquad \frac{d\dot{r}'_i}{dt'} = -\frac{1}{m_i} \cdot \frac{\partial H}{\partial r'_i}$$

- eqns for the additional DoF:

$$\frac{ds}{dt'} = \frac{1}{Q} \cdot \frac{\partial H}{\partial \dot{s}'} \qquad \frac{d\dot{s}'}{dt'} = -\frac{1}{Q} \cdot \frac{\partial H}{\partial s'}$$

Nosé–Hoover thermostat

- we obtain these eqns of motion:

$$\ddot{r}_i' = \frac{F_i}{m_i} \cdot \frac{1}{s^2} - \frac{2\dot{s}'}{s} \cdot \dot{r}_i'$$

black – usual Newtonian eqns of motion

red – bath s incorporated into the propagation,
rather than correcting velocities a posteriori

- one more eqn of motion – for the bath coordinate s :

$$\ddot{s}' = \frac{1}{Qs} \left(\sum_i m_i s^2 \dot{r}_i'^2 - g \cdot kT_{\text{ref}} \right)$$

Nosé–Hoover thermostat

such eqns are impractical because

- they work with transformed velocities \dot{r}' and accelerations \ddot{r}'
- time steps are not equally long ($\Delta t' = s \cdot \Delta t$)

to make things clearer, we

- return from the modified time scale t' to the usual t
- transform the eqns to the usual variables \dot{r} , \ddot{r}
- for the ‘velocity of bath’: pass from \dot{s} to $\gamma = \frac{\dot{s}}{s}$

Nosé–Hoover thermostat

final form of the eqns of motion:

$$\ddot{r}_i = \frac{F_i}{m_i} - \gamma \cdot \dot{r}_i$$

2nd term: formally – a kind of ‘friction’ (bath)

$$\dot{\gamma} = \frac{1}{Q} (T - T_{\text{ref}})$$

note: $\sum_i \frac{1}{2} m_i \dot{r}_i^2 = 3N \cdot \frac{1}{2} kT$

Nosé–Hoover thermostat

- strength of coupling controlled by Q – more intuitively **time τ** :

$$Q = \frac{\tau^2 \cdot T_{\text{ref}}}{4\pi^2}$$

- meaning of **period of oscillation** of the kinetic energy
- difference between τ in Berendsen and in Nosé–Hoover:
 - Berendsen – exponential damping of ΔT with τ
 - Nosé–Hoover – oscillatory relaxation of T with period τ
- N–H thermostat – incorporated in eqns of motion
 - inseparable part of the integrator,
rather than an a posteriori correction
- generates canonical phase-space density, used frequently

Andersen thermostat

from time to time, some particles (atoms) are selected randomly to undergo a 'collision' with the particles of a heat bath, which changes their velocities suddenly

this algorithm has a **stochastic** character:

- start MD with a standard integrator (Verlet. . .)
- select randomly the atoms that shall be hit by the bath
- for these atoms, draw new velocities from Maxwell–Boltzmann distribution, and keep all of the other atoms untouched

Andersen thermostat

advantage: generates canonical ensemble (if implemented right)

- rate of collisions must be neither too low (inefficient)
nor too high (collisions would dominate over eqns of motion)

disadvantage: no continuity of momentum

- dynamic properties incorrect (diffusion, viscosity. . .)

MD simulations of a molecule / molecular complex **in vacuo**

- Verlet integrator: no energy flow between modes of motion
 - equipartition of energy possibly violated
- Andersen thermostat is a viable solution
(other stochastic algorithms applicable, see further on)

Langevin dynamics

a.k.a. stochastic dynamics

additional terms in the eqns of motion:

$$m_i \ddot{\vec{r}}_i = \vec{F}_i - m_i \gamma \dot{\vec{r}}_i + \sqrt{\frac{2m_i \gamma k T}{\Delta t}} \vec{R}_i(t)$$

- velocity-dependent friction $m_i \gamma \dot{\vec{r}}_i$ (removes energy)
 - shall be $\gamma \Delta t \ll 1$, related to diffusivity: $D = kT/m\gamma$
 - frictional drag (like, of solvent imposed on a solute)
- random force or noise \vec{R}_i (adds energy)
 - from a standard normal distribution,
uncorrelated in time and across particles
 - if higher T desired \rightarrow larger additional force required
 - random collisions (like, with solvent molecules)

modified eqns of motion \rightarrow the integrator has to be modified

Brownian dynamics

overdamped Langevin dynamics, or dynamics without inertia

– no acceleration takes place, $\ddot{\vec{r}}_i = \vec{0}$:

$$\cancel{m_i} \ddot{\vec{r}}_i = \vec{F}_i - m_i \gamma \dot{\vec{r}}_i + \sqrt{\frac{2m_i \gamma k T}{\Delta t}} \vec{R}_i(t)$$

$$\dot{\vec{r}}_i = \frac{\vec{F}_i}{m_i \gamma} + \sqrt{\frac{2kT}{m_i \gamma \Delta t}} \vec{R}_i(t)$$

- 1st order ODE – integration: $\vec{r}_i(t + \Delta t) = \vec{r}_i(t) + \dot{\vec{r}}_i(t) \Delta t$
- over-damped \rightarrow long time step Δt possible
- very different from explicit all-atom MD simulation
- applications: large molecules without explicit solvent
polymers, proteins, nucleic acid molecules, colloid systems

Controlling temperature

Summary

- scaling of velocities (Berendsen, v-rescale)
- extended Lagrangian (Nosé–Hoover)
- stochastic algorithms (Andersen, Langevin)

Introducing pressure

Chemical reality – constant pressure rather than constant volume

How to calculate pressure?

From the (generalized) equipartition theorem:

$$\frac{1}{3} \left\langle \sum_i \vec{r}_i \cdot \vec{F}_i^{\text{tot}} \right\rangle = \frac{1}{3} \left\langle \sum_i \vec{r}_i \left(\vec{F}_i + \vec{F}_i^{\text{ext}} \right) \right\rangle = -NkT$$

\vec{F}_i^{ext} – force due to external pressure:

$$\frac{1}{3} \left\langle \sum_i \vec{r}_i \cdot \vec{F}_i^{\text{ext}} \right\rangle = -PV$$

\vec{F}_i – force from interactions between atoms

introduce the **virial of force**:

$$\Xi = -\frac{1}{3} \sum_i \vec{r}_i \cdot \vec{F}_i$$

Introducing pressure

Adding the components of forces:

$$-NkT = -PV - \langle \Xi \rangle$$

Consider 'instantaneous' temperature and pressure from now on:

$$\begin{aligned} -NkT &= -PV - \Xi \\ P &= \frac{NkT}{V} - \frac{1}{V}\Xi = \frac{2}{3}E_{\text{kin}} - \frac{1}{V}\Xi \end{aligned}$$

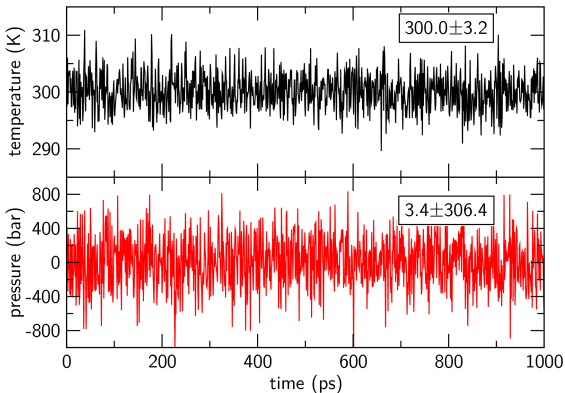
Pass to pairwise forces \vec{F}_{ij} between atoms on distances \vec{r}_{ij} :

$$\Xi = -\frac{1}{3} \sum_i \vec{r}_i \vec{F}_i = -\frac{1}{3} \sum_{i < j} \vec{r}_{ij} \vec{F}_{ij}$$

$$P = \frac{1}{3V} \left(\sum_i m_i |\vec{v}_i|^2 + \sum_{i < j} \vec{r}_{ij} \vec{F}_{ij} \right)$$

Measuring pressure

- no mention of the idea of particles colliding with the wall
- virial pressure fluctuates greatly and may even be negative:



(DNA oligomer in water at $T_{\text{ref}} = 300$ K, $P_{\text{ref}} = 1.0$ bar)

Controlling pressure

we can **calculate** the pressure

– so how do we **maintain** it at a constant value?

barostat – algorithm that is equivalent of a thermostat,
just that it varies **volume** of the box instead of velocities

the scaling of the volume is usually **isotropic**,

except for special systems (e.g. membranes)

it shall be semi-isotropic ($xy+z$) for such geometries

several options are available:

Berendsen barostat

- equivalent to the Berendsen thermostat
- molecular system coupled to a 'force / pressure bath' – piston
- direct rescaling of box lengths and atom coordinates:

$$\mu = 1 - \frac{\beta}{3} \frac{\Delta t}{\tau} (P_{\text{ref}} - P)$$
$$\vec{r}_i^j = \mu \cdot \vec{r}_i$$

- β – compressibility; $\beta = 0.000045 \text{ bar}^{-1}$ for H_2O

Parrinello–Rahman barostat

- extended-ensemble barostat – much like Nosé–Hoover algo.
- eqns of motion contain box lengths b as additional DoFs:

$$\ddot{r}_i = \frac{F_i}{m_i} - \frac{\dot{b}}{b} \cdot \dot{r}_i$$

- additional eqn of motion for the dimensions of the box:

$$\ddot{b} = \frac{V}{b} \cdot W^{-1} \cdot (P - P_{\text{ref}})$$

- strength of coupling – due to mass parameter W^{-1} :

$$W^{-1} = \frac{4\pi^2}{3} \frac{\beta}{\tau^2} \frac{1}{L}$$

τ – relaxation time (parameter)